



# Technical Appendix 2.7: Noise Impact Assessment

Kirknewton Solar & BESS EIA Report

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## Acronyms and Abbreviations

NSR	Noise Sensitive Receptor
NMP	Noise Monitoring Position
dB	Decibel
WLC	West Lothian Council
BESS	Battery Energy Storage System
BPM	Best Practicable Means
CEMP	Construction Environmental Management Plan
SMSFBS	Selms Muir Solar Farm and Battery Storage



# 1. Noise

## 1.1 Executive Summary

1.1.1 This assessment considers potential noise impacts from the Proposed Development on nearby noise sensitive receptors (NSRs). Noise impacts were assessed against the criteria outlined in BS4142 and Local Authority guidance.

1.1.2 A baseline noise survey was conducted at three noise monitoring positions (NMPs) and determined that the baseline noise environment is generally quiet, with limited influence from anthropogenic noise sources.

1.1.3 Operational noise from the Proposed Development has been predicted in noise modelling software CadnaA and it was found that the worst-case operational noise level at NSRs is below the representative daytime background and therefore noise impacts are not significant, and no additional mitigation is required.

1.1.4 Operational noise from the Proposed Development is less than 5 dB above the representative night-time background level and therefore noise impacts are not significant, and no additional mitigation is required.

1.1.5 As no additional mitigation is required, residual effects remain unchanged and are not significant.

## 1.2 Introduction

1.2.1 This assessment considers the potential effects of the Proposed Development on receptors sensitive to noise during the operational phase. Vibration associated with the Proposed Development will be negligible at sensitive receptors, given that the construction of solar and battery energy storage system (BESS) developments does not require the use of heavy plant and there are no significant sources of vibration during the operational phase, therefore assessment of vibration has been scoped out.

1.2.2 The scope of this assessment has comprised:

- Consultation with West Lothian Council (WLC) Environmental Health Department via an Environmental Impact Assessment (EIA) screening opinion, to agree appropriate scope for the assessment (refer to **Table 1** for details);
- Baseline survey to characterise existing noise levels;
- Prediction of operational noise levels in modelling software CadnaA;
- Evaluation of predicted noise levels during operation of the Proposed Development against the adopted criteria; and
- Specification of appropriate mitigation (if required).

1.2.3 Noise emissions from the operational phase of the Proposed Development will predominantly arise from the BESS element. The solar array will utilise inline



inverters, rather than centralised large inverters; inline inverters produce very little to no noise.

1.2.4 This Technical Assessment report is supported by the following Figures and Appendices:

- **Figure 1** – Site Location, Noise Monitoring Positions and Noise Sensitive Receptors;
- **Annex 1** – Baseline data and analysis; and
- **Annex 2** – Third Octave Predicted Noise Levels.

## 1.3 Legislation, Policy and Guidance

1.3.1 Relevant legislation and guidance documents have been reviewed and considered as part of this assessment. Documents of relevance are summarised below.

1.3.2 In lieu of any specific legislation, assessing the effect of operation of such a development must draw on information from a variety of sources. This assessment makes reference to several British Standards, official planning policy and advice notes and national guidance.

1.3.3 For a development of this nature, there is no specific all-encompassing legislation relating to the standards associated with noise emission/effects. Noise legislation, where it does exist, tends to be either EU-derived and focussed on specific items of noise-emitting plant or on more general nuisance, such as that addressed by the provisions of the Environmental Protection Act 1990 (UK Government, 1990).

### Legislation

#### Environmental Protection Act 1990

1.3.4 Section 79 of the Environmental Protection Act 1990 defines statutory nuisance with regard to noise and determines that local planning authorities have a duty to detect such nuisances in their area and, where a complaint of statutory nuisance is made to it by a person living within its area, to take such steps as are reasonably practicable to investigate the complaint.

1.3.5 The Act also defines the concept of “Best Practicable Means” (BPM):

- ‘practicable’ means reasonably practicable having regard among other things to local conditions and circumstances, to the current state of technical knowledge and to the financial implications;
- the means to be employed include the design, installation, maintenance and manner and periods of operation of plant and machinery, and the design, construction and maintenance of buildings and structures;
- the test is to apply only so far as compatible with any duty imposed by law; and
- the test is to apply only so far as compatible with safety and safe working conditions, and with the exigencies of any emergency or unforeseeable circumstances.



1.3.6 Section 80 of the Environmental Protection Act 1990 provides local planning authorities with powers to serve an abatement notice requiring the abatement of a nuisance or requiring works to be executed to prevent their occurrence. It is a potential defence against failure to comply with an abatement notice where BPM were used to prevent or counteract the effects of the nuisance.

### **Planning Policy**

1.3.7 The Planning Statement associated with this application sets out the planning policy framework that is relevant to the EIA. This section considers the relevant aspects of National Planning Framework 4 (NPF4), Planning Advice Notes, the West Lothian Council Local Development Plan (LDP) and other relevant guidance. Of relevance to the assessment presented within this chapter, regard has been had to the following policies:

#### **NPF4:**

1.3.8 NPF4 - Policy 11:

*“a) Development proposals for all forms of renewable, low-carbon and zero emissions technologies will be supported. These include:*

*iii. energy storage, such as battery storage and pumped storage hydro;*

*...*

*v. solar arrays;*

*...*

*e) In addition, project design and mitigation will demonstrate how the following impacts are addressed:*

*i. impacts on communities and individual dwellings, including, residential amenity, visual impact, noise and shadow flicker;”*

1.3.9 NPF4 – Policy 23:

*“Development proposals that are likely to raise unacceptable noise issues will not be supported. The agent of change principle applies to noise sensitive development. A Noise Impact Assessment may be required where the nature of the proposal or its location suggests that significant effects are likely.”*

### **Guidance**

#### **Planning Advice Note PAN 1/2011: Planning and noise**

1.3.10 PAN 1/2011 (Scottish Government, 2011), sets out a series of noise issues for planning authorities to consider when making decisions on planning applications. A Technical Advice Note (TAN) on Assessment of Noise (Scottish Government, 2011) has been published to accompany PAN 1/2011. In Appendix 1 of the TAN are codes



of practice for the assessment of various sources of noise. BS4142 is identified as appropriate guidance for the evaluation of industrial and commercial noise sources.

- 1.3.11 The TAN recommends that the daytime period includes the hours 07:00 – 23:00 and the night-time period 23:00 – 07:00.
- 1.3.12 The TAN suggests that equivalent continuous noise level over a time period, T ( $L_{Aeq,T}$ ), is a good general purpose index for environmental noise; this index is commonly referred to as the “ambient” noise level. It further notes that road traffic noise is commonly evaluated using the  $LA10,18hr$  level, and the  $LA90,T$  index is used to describe the “background” noise level.

### **BS4142:2014+A1:2019 Methods for Rating and Assessing Industrial and Commercial Sound**

- 1.3.13 BS4142:2019 describes methods for rating and assessing sound from industrial or commercial premises. The methods detailed in the standard use outdoor sound levels to assess the likely effects on people inside or outside a residential dwelling upon which sound is incident.
- 1.3.14 The standard provides methods for determining the following:
  - Rating levels for sources of industrial and commercial sound;
  - Ambient, background and residual sound levels; and
  - The audibility of tones in sound: 1/3 octave method.
- 1.3.15 These may be used for assessing sound from proposed, new, modified or additional sources of sound of a commercial or industrial nature or to assess the suitability of introducing a receptor near an existing commercial or industrial site.
- 1.3.16 The standard makes use of the following terms:
  - Ambient sound level,  $L_a = L_{Aeq,T}$  – the equivalent continuous sound pressure level of the totally encompassing sound in a given situation at a given time, usually from multiple sources, at the assessment location over a given time interval, T.
  - Background sound level,  $L_{A90,T}$  – the A-weighted sound pressure level that is exceeded by the residual sound at the assessment location for 90 percent of a given time interval, T, measured using time weighting F and quoted to the nearest whole number of decibels.
  - Specific sound level,  $L_s = L_{Aeq,Tr}$  – the equivalent continuous sound pressure level produced by the specific sound source at the assessment location over a given reference time interval, T.
  - Rating level,  $L_{Ar,Tr}$  – the specific sound level plus any adjustment for the characteristic features of the sound.
  - Residual sound level,  $L_r = L_{Aeq,T}$  – the equivalent continuous sound pressure level at the assessment location when the specific sound source is suppressed to such a degree that it does not contribute to the ambient sound, over a given reference time interval, T.



1.3.17 The standard determines the degree of noise impact by comparison of the background noise level at noise sensitive receptors (NSRs) in the absence of the industrial or commercial facility (the specific source) with the ambient sound level when the specific source is operational.

1.3.18 Where particular characteristics such as tones, intermittency or impulsivity are present in the noise emissions of the specific source and perceptible at the receptor, the standard requires that “penalties” be added to the specific sound level to account for the increased annoyance that these can cause.

1.3.19 The following evaluation impact significance identifiers are provided in the standard, in which the difference between the specific sound level and measured background level are considered:

- the greater the difference, the greater the magnitude of impact;
- a difference of around +10 dB or more is likely to be an indication of a significant adverse impact, depending on the context;
- a difference of around + 5 dB is likely to be an indication of an adverse impact, depending on the context;
- the lower the rating level, relative to the measured background level, the less likely that the specific sound source will have an adverse (or significant adverse) impact; and
- where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact.

1.3.20 The standard also makes the following comments:

*“Where the initial estimate of the impact needs to be modified due to the context, take all pertinent factors into consideration, including the following:*

**1. The absolute level of sound. For a given difference between the rating level and the background sound level, the magnitude of the overall impact might be greater for an acoustic environment where the residual sound level is high than for an acoustic environment where the residual sound level is low.**

**Where background sound levels and rating levels are low, absolute levels might be as, or more, relevant than the margin by which the rating level exceeds the background. This is especially true at night.**

**Where residual sound levels are very high, the residual sound might itself result in adverse impacts or significant adverse impacts, and the margin by which the rating level exceeds the background might simply be an indication of the extent to which the specific sound source is likely to make those impacts worse.**

**2. The character and level of the residual sound compared to the character and level of the specific sound. Consider whether it would be beneficial to compare the frequency spectrum and temporal variation of the specific sound with that of the ambient or residual sound to assess the degree to which the specific sound source is likely to be distinguishable and will represent an incongruous sound by comparison to the acoustic environment that would occur in the absence of the specific sound. Any sound parameters, sampling periods and averaging time periods used to undertake character comparisons should reflect the way in which**



*sound of an industrial and/ or commercial nature is likely to be perceived and how people react to it.*

*3. The sensitivity of the receptor and whether dwellings or other premises used for residential purposes will already incorporate design measures that secure good internal and/or outdoor acoustic conditions, such as:*

- *facade insulation treatment;*
- *ventilation and/or cooling that will reduce the need to have windows open so as to provide rapid or purge ventilation; and*
- *acoustic screening.”*

1.3.21 Whilst the latest revision of BS 4142 does not provide definition of low or very low background and rating levels the previous (1997) version considered that background levels of 30 dBA and rating levels of 35 dBA could be considered low.

1.3.22 Numerous studies by Moorhouse, Berry, Flindell, etc for the Health Protection Agency and for Defra (referenced within the Further Reading Section of BS 4142) and supported by the recent Association of Noise Consultants Working Group report on BS4142 application (Association of Noise Consultants, March 2020) conclude that impacts at rating levels below 35 dB are unlikely.

1.3.23 At night, particularly, where potential sleep disturbance is the key issue, a rating level of below 35 dB results in internal levels significantly below the BS 8233 guideline values.

#### **ISO 9613; Attenuation of sound during propagation outdoors, Part 1 and Part 2**

1.3.24 ISO 9613 1&2 describe a method for calculating the attenuation of sound during propagation outdoors in order to predict the levels of environmental noise at a distance from a variety of sources. The method predicts the equivalent continuous A-weighted sound pressure level under meteorological conditions.

## **1.4 Consultation**

1.4.1 **Table 1** provides details of consultations undertaken with relevant regulatory bodies, together with action undertaken by the Applicant in response to consultation comments.

**Table 1: Consultation Relevant to Noise and Vibration**

Consultee	Key Consultee Comments	Application Action
West Lothian Council (WLC) (4 <sup>th</sup> September 2025)	WLC EIA screening opinion submitted.	Acknowledgment from WLC to respond by 3 November 2025.



Consultee	Key Consultee Comments	Application Action
WLC (9 <sup>th</sup> October 2025)	WLC screening response received. WLC request a noise assessment. Specifically, “ <i>you may wish to discuss this with our Environmental Health team regarding the form of any potential noise protection. Note that likely effects will be during construction.</i> ”	Undertake a noise assessment following WLC planning guidance and policies. Submit report in support of planning application.

## 1.5 Assessment Methodology and Significance Criteria

### Study Area

- 1.5.1 The Study Area considered in this assessment encompasses the land within the Proposed Development boundary and the nearest residential NSRs which may be impacted upon by noise emissions from the site.
- 1.5.2 Noise levels due to the Proposed Development at more distant NSRs will be lesser than at the closest NSRs, therefore compliance with criteria at the closest NSRs will entail compliance at those more distant.

### Receptors Requiring Assessment

- 1.5.3 The nearest residential noise sensitive receptors (NSRs) to the Proposed Development have been identified and are described in **Table 2** and are shown in **Figure 1**.

**Table 2: NSRs considered in this assessment**

NSR ID	Description	X	Y
NSR1	Residential – Newlands, EH17 8LR	311223.44	665171.13
NSR2	Residential – Leyden Road, EH27 8DQ	310588.98	664308.77
NSR3	Residential – Leyden Road, EH27 8DQ	310005.91	665398.10
NSR4	Residential – Leyden Road, EH27 8DQ	309855.40	664573.72
NSR5	Hilly Cow Wigwams, Leyden Road, EH27 8DQ	309927.80	664357.13

### Desk Study

#### Prediction of Operational Noise Levels

- 1.5.4 Noise levels potentially generated by the Proposed Development have been predicted at identified representative NSRs within noise modelling software CadnaA, using the propagation method set out in ISO9613. The model assumes soft ground conditions, with absorption set to G=1.0, except for the BESS compound which is set to G=0 (hard ground), and the land containing the PV panels is set to G=0.6 (mixed ground). The model considers screening provided by local topography in the form of 1 m resolution digital terrain mapping (DTM) data. A



typical air temperature of 10°C and relative humidity of 70% have been assumed within the model.

1.5.5 Although the exact equipment specification and technology provider is unknown at this time, the Applicant has confirmed that the CATL EnerC+ battery unit and PE GEN3 Inverter are appropriate for use as indicative items of plant for this assessment.

- Inverters, 2 no. – Power Electronics HEMK/PCSK GEN3 INVERTER, Sound Optimised, total modelled Sound Power Level 83.6 dB(A) per unit
- Batteries, 4 no. – CATL Ener C+, total modelled Sound Power Level 80.3 dB(A) per unit
- Transformers, 1 no. within the BESS and 7 within the solar array – total modelled Sound Power Level 79.7 dB(A) per unit

1.5.6 The batteries and inverters have been modelled as 3D objects, with their noise emissions coming from area sources and vertical area sources which represent the tops and sides of the units. Transformers have been modelled as point sources.

1.5.7 For the source data of the transformers, we have applied spectral data for a transformer, obtained during noise monitoring of an operational BESS site. Noise test reports for the batteries and inverter have been supplied by the manufacturer, and verification modelling undertaken in which the test scenario for each item of equipment has been recreated in CadnaA.

1.5.8 In the verification modelling, receivers have been placed at the same locations as the reported microphone positions. The reported 1/3 octave-band sound power levels of the equipment have been entered as source data, and where necessary the sound power levels of the individual area sources/vertical area sources have been adjusted equally in each frequency band so that the predicted sound pressure levels at the receivers match as closely as possible to the reported sound pressure levels during the tests.

1.5.9 NSRs have been modelled as a receiver placed on the closest approach to the Proposed Development.

1.5.10 The sound power levels for the BESS equipment are shown in **Table 3** as octave-band data. The octave band spectra have been normalised within the model to the A-weighted sound power level, following the verification exercise.

**Table 3: Sound Power Levels**

Item	Octave Band Sound Power Level (centre frequency in Hz), dB								Normalised Sound Power Level, dB(A)
	63	125	250	500	1k	2k	4k	8k	
CATL EnerC+	75.3	78.6	79.7	77.8	76.5	71.7	67.2	67	80.3
PE Gen3 Inverter	80.5	91.5	78.5	71	70.1	68.7	69.3	68.4	83.6
Transformer	31.3	44.3	31.8	34.3	28.6	21	12.9	1.3	79.7



1.5.11 The actual model of battery and inverter plant installed will depend on the outcome of a tendering process. This assessment therefore considers representative candidate plant, noting that the installed plant may be different. Battery and inverter technology is currently developing at a rapid pace, and noise is often a primary constraint in the UK market. Technology providers are therefore delivering units with increasingly improved noise performance. It is therefore reasonable to assume that by the time the Proposed Development is ready to build, following planning consent and becoming operational, quieter plant than the candidate considered in this assessment will be available.

### Rating Levels

1.5.12 BS4142 requires consideration of potential character corrections that may be applied to noise from the BESS. When determining whether any character corrections should apply to the Specific Level for deriving the Rating Level, in accordance with BS4142, this assessment notes the following:

- the 1/3 octave spectral data at each receptor have been tested for potential tonal components in accordance with the third octave method referenced in BS4142 and found to be non-tonal (see **Annex 2**);
- operation of the BESS will not result in impulsive characteristics;
- the operational profile of the BESS was considered;
- the site will produce noise only whilst the batteries are charging or discharging and will be effectively silent at other times. Charging and discharging occurs for periods of >1 hour at a time, i.e. reasonably prolonged, and greater than the BS4142 reference periods for daytime and night-time;
- it is therefore considered that noise from the site will not have intermittent characteristics; and,
- on the basis of the above, no corrections have been applied, and the Rating Level is therefore equal to the predicted Specific Level.

### Baseline Noise Survey

1.5.13 SLR Consulting undertook a baseline survey between Friday 20th June 2025 and Thursday 26th June 2025, encompassing weekday and weekend periods. Monitoring was undertaken in accordance with BS 4142 and BS 7445, using Rion NL-52 Class I integrating sound level meters (SLM). Conditions were mainly calm and dry at the time of the survey, with intermittent precipitation periods. Any non-compliant weather periods were omitted from the collected datasets.

1.5.14 The SLMs were within their laboratory calibration period, and a calibration check was performed before and after each measurement, with no drift in calibration noted.

1.5.15 Monitoring was undertaken at three noise monitoring positions (NMPs) to characterise the noise environments at the NSRs.

- NMP1, north-west of the site, within the front garden of NSR3



- NMP2, at the southwestern boundary of the site, representative of NSR2, NSR4, and NSR5
- NMP3, at the eastern boundary of the site, representative of NSR1

1.5.16 Unattended long-term measurements were undertaken for a period of approximately six days.

1.5.17 The long term NMPs were located at the closest points of the site to the NSRs and were positioned to provide security for the monitoring equipment. Observations by the surveyor confirmed that the NMPs were suitably representative of the noise environment at the NSRs.

1.5.18 The monitoring positions are shown in **Figure 1**.

1.5.19 **Table 4** presents a summary of the results of the baseline survey. Further details of the measured baseline noise are presented in **Annex 1**.

**Table 4: Measured sound levels**

NMP	Period	$L_{Aeq,T}$ dB	$L_{Amax,T}$ dB	$L_{A10,T}$ dB	$L_{A90,T}$ dB
Daytime					
NMP1	18:05 20/06/2025 – 13:55 26/06/2025	51	89	48	35
NMP2	17:59 20/06/2025 – 14:19 26/06/2025	52	95	48	39
NMP3	17:39 20/06/2025 – 14:39 26/06/2025	55	90	49	41
Night					
NMP1	23:00 20/06/2025 - 07:00 26/06/2025	45	83	41	31
NMP2	23:00 20/06/2025 - 07:00 26/06/2025	45	80	40	32
NMP3	23:00 20/06/2025 - 07:00 26/06/2025	47	75	44	36

1.5.20 Statistical analysis examining the cumulative distribution of the measured background sound levels,  $L_{A90}$ , has been undertaken in order to derive a representative background sound level (see **Annex 1**) at each NSR.

**Table 5: Representative background sound level**

NMP/NSR	Daytime, $L_{A90,T}$ , dB	Night-time, $L_{A90,T}$ , dB
NMP1 / NSR3	35 (34)*	31
NMP2 / NSR2, NSR4, NSR5	39	32
NMP3 / NSR1	41	36
<b>Note:</b> *Based on omitting noisy events (helicopter/agricultural activity) from resident's diary		



## Assessment of Likely Significance

1.5.21 Noise impacts have been determined with reference to BS4142 guidance. The specific noise level resulting from the operation of the Proposed Development has been predicted at identified representative NSRs.

1.5.22 The guidance contained within Technical Advice Note to PAN 1/2011 has been used to adopt an appropriate set of significance criteria. The receptor sensitivity criteria considered in this assessment are presented in **Table 6**.

**Table 6: NSR Sensitivity**

Receptor Sensitivity	Description	Examples
High	Receptors where people or operations are particularly susceptible to noise.	Residential, quiet outdoor recreational areas, schools and hospitals.
Medium	Receptors moderately sensitive to noise, where it may cause some distraction or disturbance.	Offices and restaurants.
Low	Receptors where distraction or disturbance from noise is minimal.	Buildings not occupied, factories and working environments with existing levels of noise.

1.5.23 This assessment considers all identified NSRs to be of high sensitivity, given that they are residential dwellings.

1.5.24 The significance of operational noise from the Proposed Development has been determined based on the guidance contained within BS4142, i.e. by consideration of the difference between the rating level and the prevailing background sound levels, with respect to context and the resulting sound levels in absolute terms.

1.5.25 The impact magnitudes associated with operational noise from the Proposed Development are presented in **Table 7**.

**Table 7: Noise Impact Magnitude**

Difference, d, Between Rating Level ( $L_{Ar,Tr}$ ) and Background Sound Level ( $L_{A90}$ )	BS4142 Guidance	Adopted Impact Magnitude
$d >+10$	Indication of significant adverse impact	High
$d >+5, \leq 10$	Indication of adverse impact	Medium
$d \leq +5, > 0$	Indication of no adverse Impact	Low
$d \leq 0$	Indication of low impact	Negligible
Where the rating level ( $L_{Ar,Tr}$ ) is below 35dB the impact magnitude is classified as 'Low' or lesser, regardless of the relationship to the background noise level.		
Where predicted internal levels at NSRs are below NR25 with windows open impact magnitude is classified as low.		



1.5.26 The effect significance for operational noise has been determined by consideration of both the receptor sensitivity and the impact magnitude according to the matrix detailed in **Table 8**.

**Table 8: Effect Significance Matrix**

Impact Magnitude	Receptor Sensitivity		
	High	Medium	Low
High	Major	Moderate	Minor
Medium	Moderate	Minor	Negligible
Low	Minor	Negligible	Negligible
Negligible	Negligible	Negligible	Negligible

1.5.27 Effects with a significance of moderate and major are considered **significant**. Effects with a significance of negligible and minor are considered **not significant**.

### **Requirements for Mitigation**

1.5.28 Mitigation will be specified where significant adverse effects are identified.

### **Assessment of Residual Effect Significance**

1.5.29 Where mitigation is proposed, residual effect significance has also been determined with reference to the adopted noise criteria following specification of appropriate mitigation.

### **Assessment of Cumulative Effects**

1.5.30 An approved Solar Farm and BESS facility is proposed to be located at Selms Muir Farm, WLC planning ref: 0442\_FUL\_22. with the potential for cumulative noise effects identified within 5 km of the Proposed Development.

### **Limitations to Assessment**

1.5.31 The assessment of operational noise impacts associated with the Proposed Development has been undertaken adopting representative source noise levels for batteries, inverters and transformers. The actual plant installed will be subject to the outcome of the tendering process, however, the equipment chosen will be selected to ensure compliance with the adopted noise criteria outlined in this assessment.

## **1.6 Scope of the Assessment**

### **Impacts Scoped Out of Assessment**

1.6.1 It is considered that construction noise impacts may be minimised by appropriate controls on working hours, specification of appropriate plant and methods and



implementation of best practices and, therefore, the prediction and evaluation of construction noise is scoped out.

1.6.2 No significant sources of vibration are expected, and we have therefore scoped out further consideration of vibration during the construction and operational phases.

### **Environmental Measures Embedded into the Development Proposals**

1.6.3 The Applicant is committed to meeting appropriate noise limits, during the construction and decommissioning phase and the operational phase.

1.6.4 Appropriate noise limits for construction noise have been derived from measured baseline data, in accordance with methods provided in BS5228 as follows:

- Daytime (07:00 – 19:00) and Saturdays (07:00 – 13:00) – 65 dB  $L_{Aeq,T}$ ;
- Evenings and weekends (19.00–23.00 weekdays, 13.00–23.00 Saturdays and 07.00 – 23.00 Sundays) – 55 dB  $L_{Aeq,T}$ ; and
- Night-time (23:00 – 07:00) – 45 dB  $L_{Aeq,T}$ .

1.6.5 The limits detailed above will inform the Construction Environmental Management Plan (CEMP). Construction and environmental management plans are introduced in Chapter 4: Project Description of the EIA Report and will be secured via a condition in agreement with WLC.

1.6.6 Inverters for the solar array will be in-line inverters, rather than large, centralised inverters. In-line inverters produce little to no noise emissions.

## **1.7 Assessment of Potential Effects**

### **Construction Effects**

1.7.1 As noted above, noise impacts during the construction phase will be limited by the implementation of a CEMP. Compliance with the noise limits will result in construction phase noise effects being **not significant**.

### **Operational Effects**

1.7.2 The predicted operational noise levels are provided and evaluated against BS4142 criteria in **Table 9**.

**Table 9: Evaluation of Operational Noise Levels**

NSR ID	Predicted Specific Noise Level, dB $L_{Aeq,T}$	Character correction, rationale	Derived rating level, dB $L_{Ar,Tr}$	Limiting rating noise level, dB $L_{Ar,Tr}$ , (background +5 dB)	Comparison with criterion, (predicted level minus limiting level), dB(A)
Daytime period (1hr)					
NSR1	26	0, no tonality, intermittency or impulsivity	26	46	-20
NSR2	17		17	44	-27
NSR3	22		22	39	-17



NSR ID	Predicted Specific Noise Level, dB $L_{Aeq,T}$	Character correction, rationale	Derived rating level, $dB\bar{L}_{Ar,Tr}$	Limiting rating noise level, $dB\bar{L}_{Ar,Tr}$ , (background +5 dB)	Comparison with criterion, (predicted level minus limiting level), dB(A)
NSR4	25		25	44	-19
NSR5	24		24	44	-20
Night-time period (15 mins)					
NSR1	27	0, no tonality, intermittency or impulsivity	27	41	-14
NSR2	19		19	37	-18
NSR3	24		24	36	-12
NSR4	27		27	37	-10
NSR5	24		24	37	-13

1.7.3 Predicted rating levels are below the BS 4142 criteria of background +5 dB at all receptors and the initial assessment of impacts, with reference to **Table 7**, indicates a low impact.

1.7.4 Predicted rating levels are also substantially below 35 dB and, with reference to **Table 7**, this also indicates a negligible impact.

**1.7.5** Predicted operational noise levels are considered in the context of a NR25 target maximum noise level for bedrooms during the night-time period in **Table 10**, **Table 11**, **Table 12**, **Table 13**, and



1.7.6 **Table 14** representing NSR1, NSR2, NSR3, NSR4, and NSR5 respectively. NSR5 is included for completeness, although this location is understood to be a holiday home, therefore a transient residency.

1.7.7 Façade corrections of +2 dB have been included within the predicted facade levels and an open window has been assumed (reduction in each octave band based on WLC guidance).

**Table 10: Evaluation of predicted night-time internal noise levels, NSR1**

	Octave Band Level, dB						
	63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz
Predicted Façade Level	32.0	39.8	26.5	24.2	21.4	12.9	-2.7
Open Window reduction (conservative)	5	5	5	10	10	10	10
Predicted Internal Level	27.0	34.8	21.5	14.2	11.4	2.9	-12.7
NR 25 curve	55.2	43.7	35.2	29.2	25	21.9	19.5
Margin of Compliance	-28.2	-8.9	-13.7	-15.0	-13.6	-19.0	-32.2



**Table 11: Evaluation of predicted night-time internal noise levels, NSR2**

	Octave Band Level, dB						
	63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz
Predicted Façade Level	30.3	32.8	20.9	15.4	10.5	1.3	-15.1
Open Window reduction (conservative)	5	5	5	10	10	10	10
Predicted Internal Level	25.3	27.8	15.9	5.4	0.5	-8.7	-25.1
NR 25 curve	55.2	43.7	35.2	29.2	25	21.9	19.5
Margin of Compliance	-29.9	-15.9	-19.3	-23.8	-24.5	-30.6	-44.6

**Table 12: Evaluation of predicted night-time internal noise levels, NSR3**

	Octave Band Level, dB						
	63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz
Predicted Façade Level	31.6	32.6	24.0	21.7	19.2	10.9	-5.4
Open Window reduction (conservative)	5	5	5	10	10	10	10
Predicted Internal Level	26.6	27.6	19.0	11.7	9.2	0.9	-15.4
NR 25 curve	55.2	43.7	35.2	29.2	25	21.9	19.5
Margin of Compliance	-28.6	-16.1	-16.2	-17.5	-15.8	-21.0	-34.9

**Table 13: Evaluation of predicted night-time internal noise levels, NSR4**

	Octave Band Level, dB						
	63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz
Predicted Façade Level	32.3	34.8	25.9	25.0	22.9	15.0	-0.6
Open Window reduction (conservative)	5	5	5	10	10	10	10
Predicted Internal Level	27.3	29.8	20.9	15.0	12.9	5.0	-10.6
NR 25 curve	55.2	43.7	35.2	29.2	25	21.9	19.5
Margin of Compliance	-27.9	-13.9	-14.3	-14.2	-12.1	-16.9	-30.1



**Table 14: Evaluation of predicted night-time internal noise levels, NSR5**

	Octave Band Level, dB						
	63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz
Predicted Façade Level	5.2	17.6	12.1	16.1	21.1	14.7	-2.1
Open Window reduction (conservative)	5	5	5	10	10	10	10
Predicted Internal Level	26.4	28.8	15.8	9.4	11.1	3.5	-13.1
NR 25 curve	55.2	43.7	35.2	29.2	25	21.9	19.5
Margin of Compliance	-28.8	-14.9	-19.4	-19.8	-13.9	-18.4	-32.6

**1.7.8** The predicted level due to operation of the facility within bedrooms meets the target NR25 level at each octave band by a substantial margin.

**1.7.9** As demonstrated in **Table 10**, **Table 11**, **Table 12**, **Table 13**, and



1.7.10 **Table 14**, the operation of the facility meets the WLC criteria for a night-time indoor noise limit of NR25. This assessment therefore considers that noise from the operation of the facility will have low impact.

1.7.11 This assessment therefore considers that noise impacts will be **not significant**.

### **Decommissioning Effects**

1.7.12 As noted above, noise impacts during the decommissioning phase will be limited by the implementation of a CEMP. Compliance with the noise limits will result in decommissioning phase noise effects being **not significant**.

## **1.8 Mitigation**

1.8.1 The assessment has demonstrated that the Proposed Development will meet the WLC criteria, therefore no additional mitigation is proposed.

## **1.9 Assessment of Residual Effects**

### **Construction**

1.9.1 No requirement for specific additional mitigation has been determined for the construction phase, therefore no additional mitigation is proposed, and residual effects remain unchanged and are **not significant**.

### **Operation**

1.9.2 No specific additional mitigation has been determined to be required for the operational phase; therefore, no additional mitigation is proposed, and residual effects remain unchanged and are **not significant**.

## **1.10 Assessment of Cumulative Effects**

1.10.1 Cumulative developments which were operational within the study area during the baseline sound survey have been considered as they form part of the existing soundscape.

1.10.2 An approved Solar Farm and BESS facility is proposed to be located at Selms Muir Farm, WLC planning ref: 0442\_FUL\_22. Potential cumulative effects from the operational Selms Muir Solar Farm and Battery Storage (SMSFBS) and Kirknewton Solar and BESS have been considered at receptor NSR3 (referred to as ESR3 in the SMSFBS noise impact assessment<sup>1</sup>). NSR3 represents the closest receptor located between both of the sites.

1.10.3 The predicted cumulative operational noise levels at NSR3 are provided and evaluated against BS4142 criteria in **Table 15**.

<sup>1</sup> Wardell Armstrong LLP (2022). Renewable Connections Developments Ltd Proposed Solar Farm and Battery Storage Development at Land at Selms Muir.



**Table 15: Evaluation of Cumulative Operational Noise Levels at NSR3**

NSR ID	Predicted Specific Noise Level, dB $L_{Aeq,T}$	Character correction, rationale	Derived rating level, dB $L_{Ar,Tr}$	Limiting rating noise level, dB $L_{Ar,Tr}$ , (background +5 dB)	Comparison with criterion, (predicted level minus limiting level), dB(A)
Daytime period (1hr)					
NSR3	22	0, no tonality, intermittency or impulsivity	22	39	-17
ESR3 (SMSFBS report)	19		19	39	-20
Combined Total	24		24	39	-15
Night-time period (15 mins)					
NSR3	24	0, no tonality, intermittency or impulsivity	24	36	-12
ESR3 (SMSFBS report)	19		19	36	-17
Combined Total	25		25	36	-11

1.10.4 Predicted rating levels are below the BS 4142 criteria of background +5 dB at the cumulative receptor NSR3 and the initial assessment of impacts, with reference to **Table 7**, indicates a negligible impact. Therefore, no cumulative operational effects are anticipated.

1.10.5 Predicted operational noise levels are considered in the context of a NR25 target maximum noise level for bedrooms during the night-time period in **Table 16** representing NSR3.

1.10.6 Façade corrections of +2 dB have been included within the predicted facade levels and an open window has been assumed (reduction in each octave band based on WLC guidance).

**Table 16: Evaluation of predicted cumulative night-time internal noise levels, NSR3**

	Octave Band Level, dB						
	63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz
Predicted Façade Level	31.9	32.9	24.5	22.2	19.7	11.3	-5.2
Open Window reduction (conservative)	5	5	5	10	10	10	10
Predicted Internal Level	26.9	27.9	19.5	12.2	9.7	1.3	-15.2
NR 25 curve	55.2	43.7	35.2	29.2	25	21.9	19.5
Margin of Compliance	-28.3	-15.8	-15.7	-17.0	-15.3	-20.6	-34.7



- 1.10.7 The predicted cumulative noise level due to operation of the facility and SMSFBS within bedrooms meets the target NR25 level at each octave band by a substantial margin.
- 1.10.8 As demonstrated in **Table 16**, the cumulative assessment meets the WLC criteria for a night-time indoor noise limit of NR25. This assessment therefore considers that cumulative noise from the operation of the facility and SMSFBS will have low impact.
- 1.10.9 This assessment therefore considers that noise impacts will be not significant.

## 1.11 Summary

- 1.11.1 Information on noise and vibration within the noise and vibration study area was collected through desktop review, site surveys and consultation.
- 1.11.2 Overall, it is concluded that there will be no likely significant residual effects arising from the Proposed Development during the construction, operational and maintenance or decommissioning phases.
- 1.11.3 Mitigation during construction will be secured within the CEMP. Mitigation measures for operational noise are not considered necessary.



## 1.12 References

BSI Publications. 2019. "BS4142:2014+A1:2019 Methods for Rating and Assessing Industrial and Commercial Sound."

BSI Publications. 2003. "BS7445:2003 Description and measurement of environmental noise, Guide to quantitites and procedures."

BSI Publications. 2014. "BS8233:2014 Guidance on sound insulation and noise reduction in buildings."

ISO. 1993. "ISO 9613 Acoustics - Attenuation of sound during propagation outdoors, Part 1: Calcualtion of the absorption of sound by the atmosphere, Part2: General method of calculation."

Scottish Government. 2024. *National Planning Framework 4*. Scottish Government.

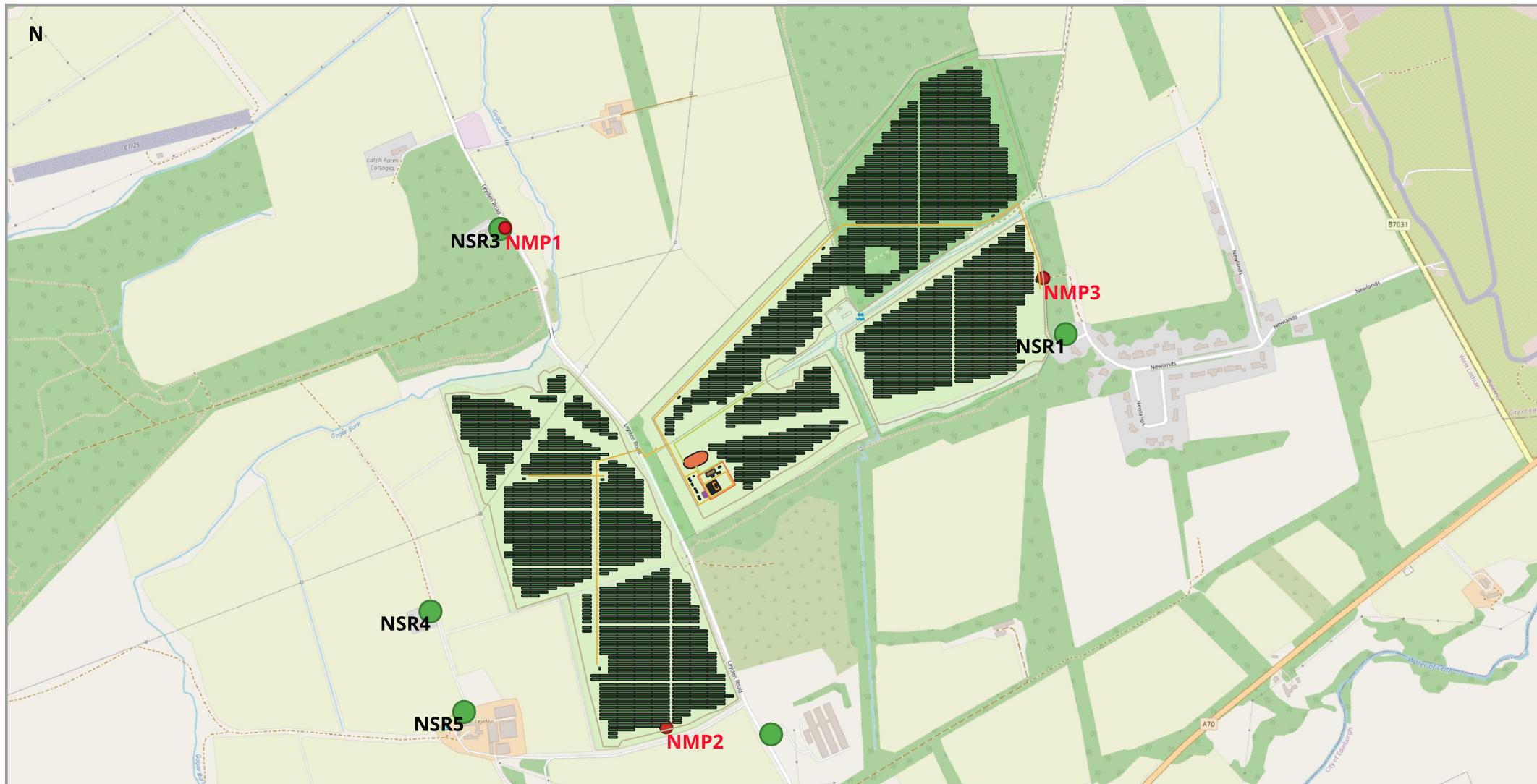
Scottish Government. 2011. *Planning Advice Note 1, PAN1/2011*. Scottish Government.

Association of Noise Consultants Good Practice Working Group, BS4142:2014+A1:2019 Technical Note, 2020



# Figure





**KEY**

- NMPs ●
- NSRs ●



Coordinate System: OSGB86  
Projection: Transverse Mercator

Service Layer Credits:  
Contains OS data © Crown Copyright and database rights 2019

0 0.01 0.02 0.03 0.04 kilometres  
Scale @ A4: 1:11,775.999057

Kirknewton Solar & BESS EIA  
Noise Impact Assessment Proposed Layout



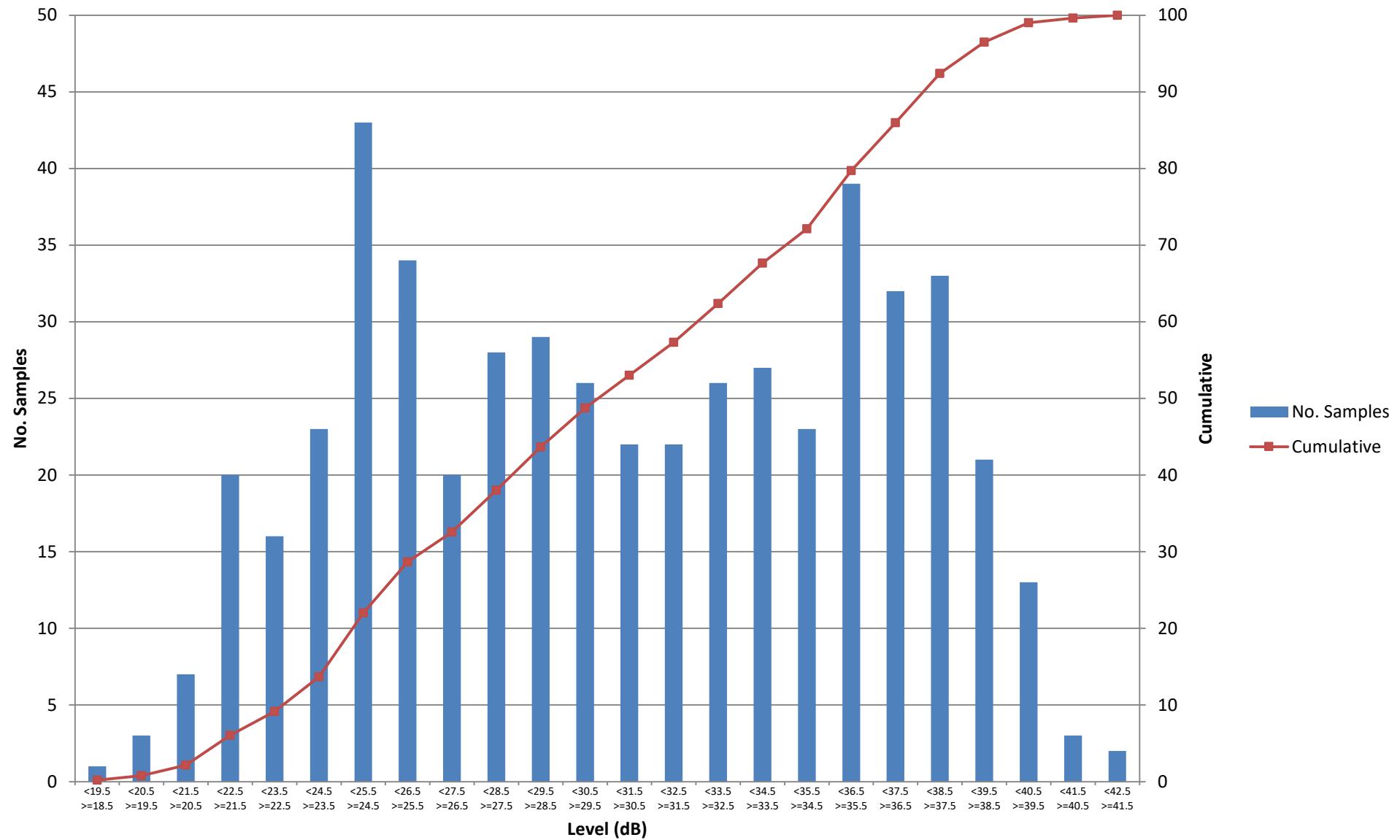
Figure 1 Proposed Layout with NSRs, NMPs

Date: 24/10/2025	Lead: DC	Review: DC	Version: v1.0
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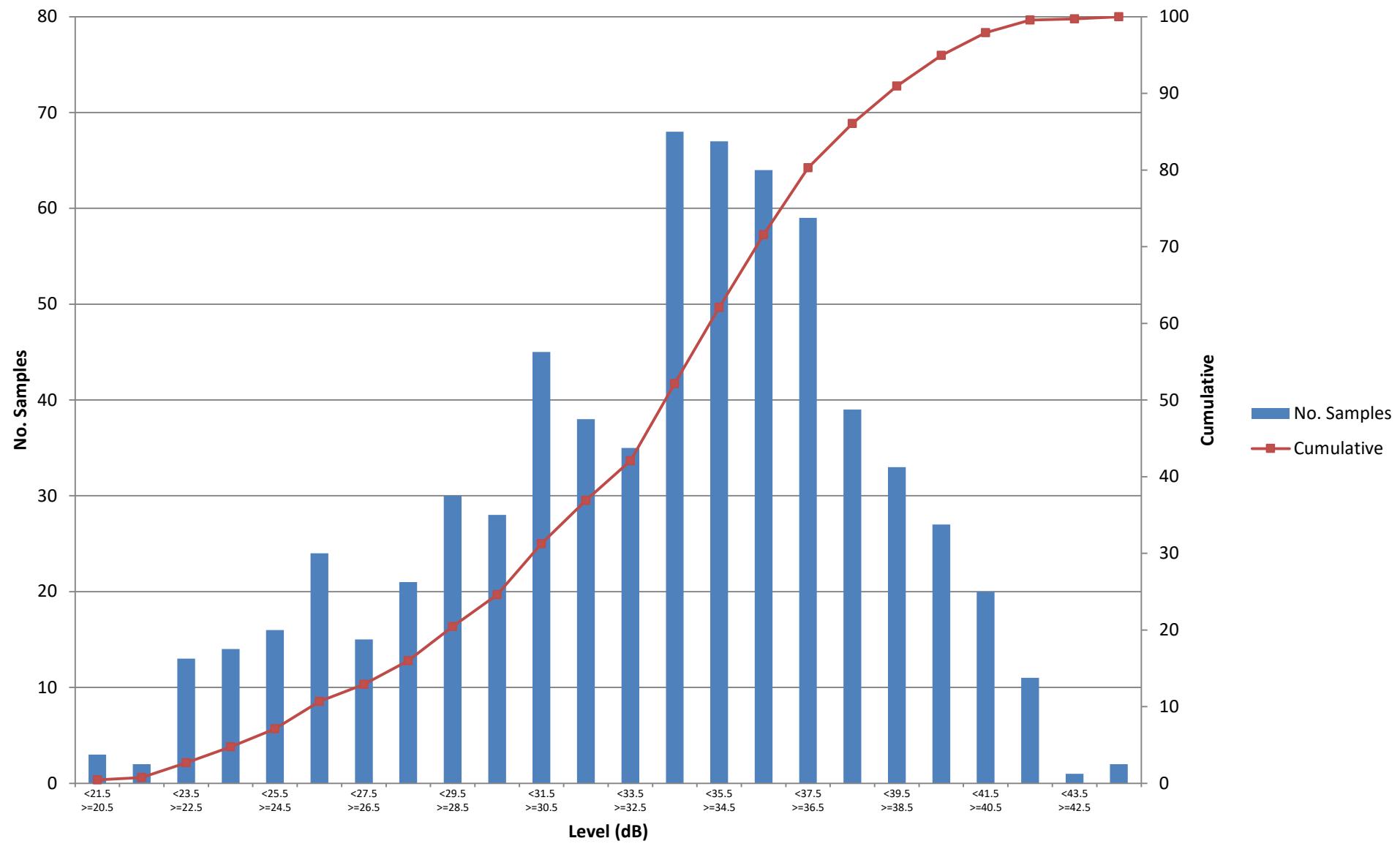
# Annex 1



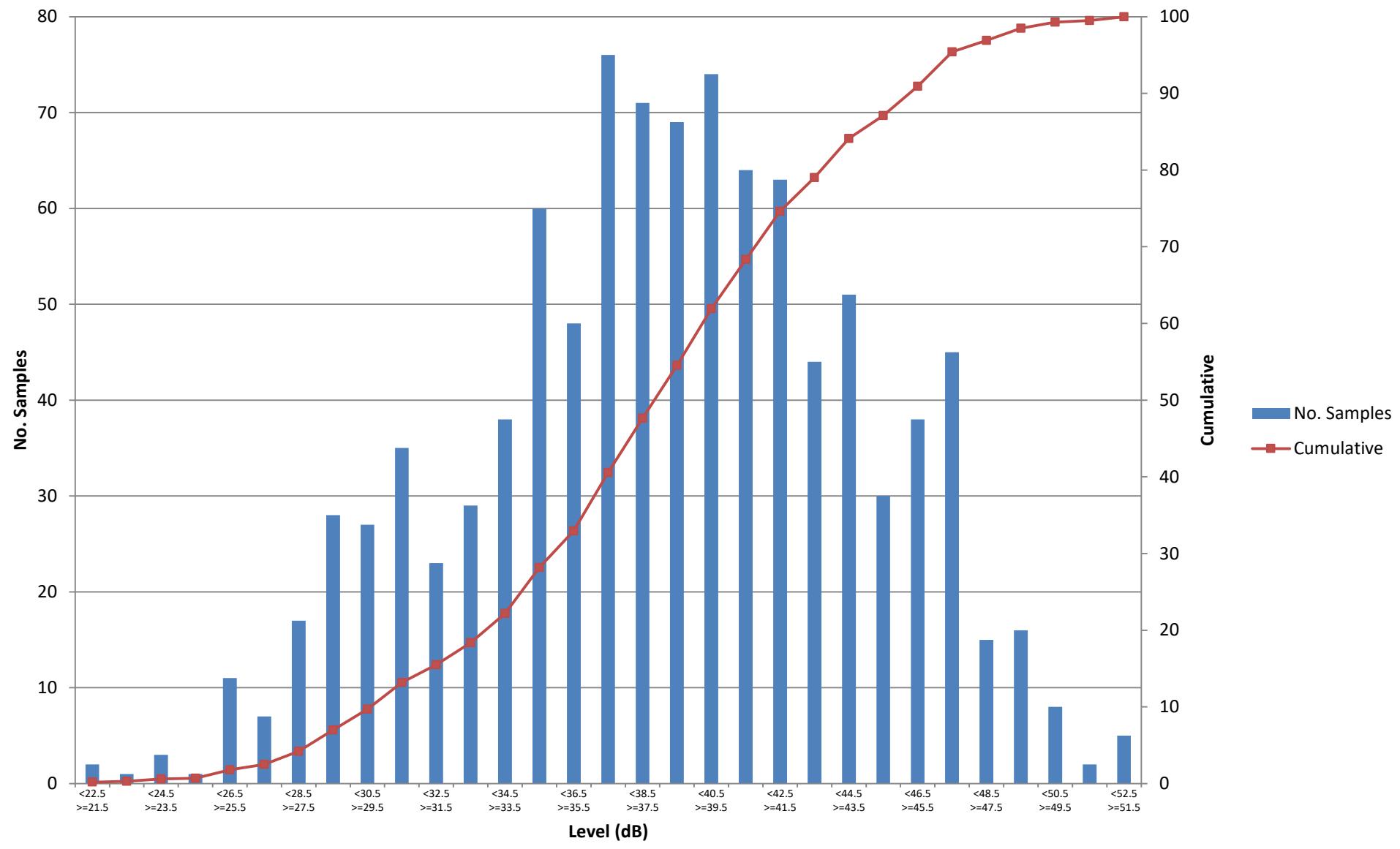
## NMP1 LA90 Night-time Histogram 20/06/25 to 26/06/25



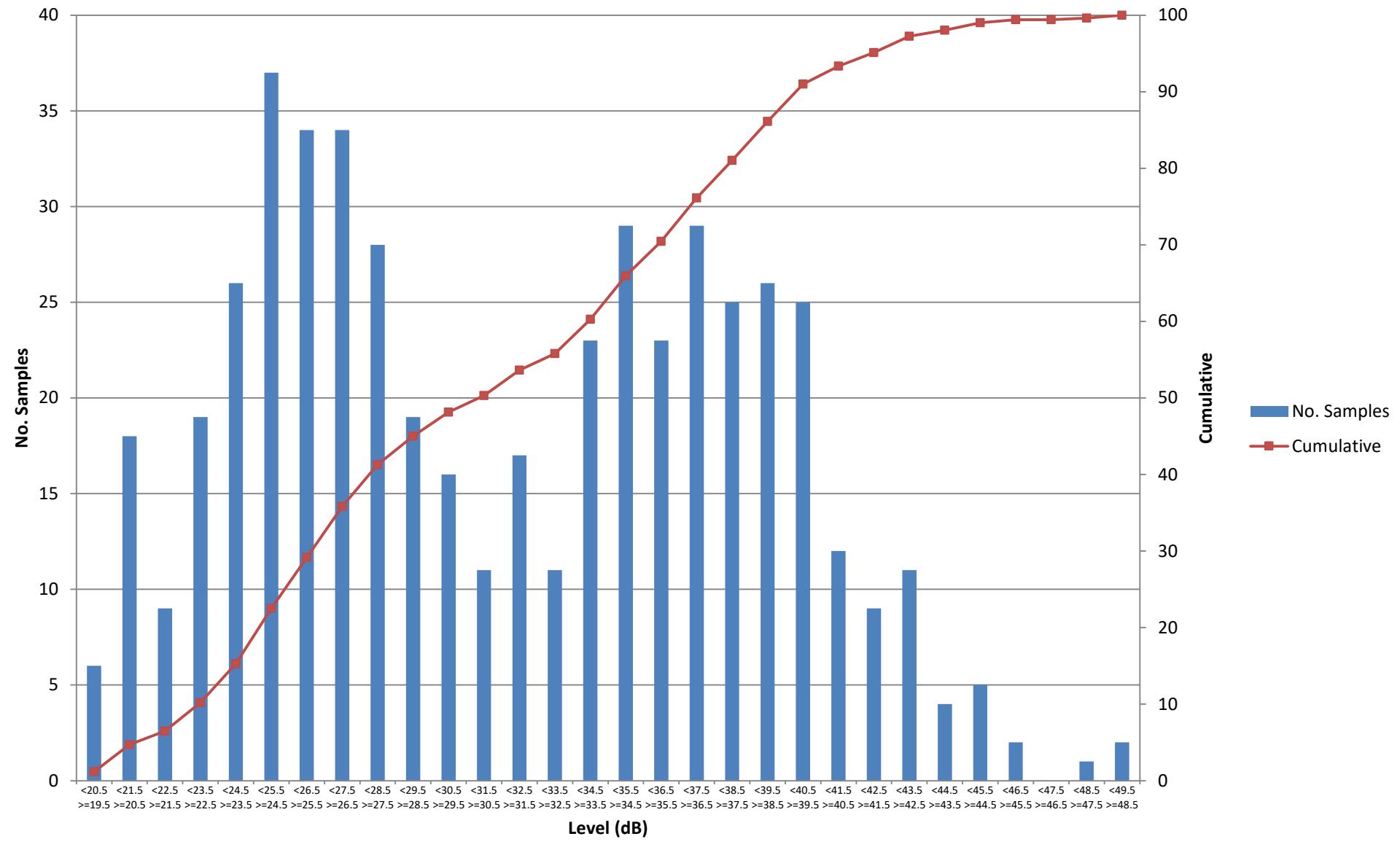
## NMP1 LA90 Daytime Histogram 20/06/25 to 26/06/25



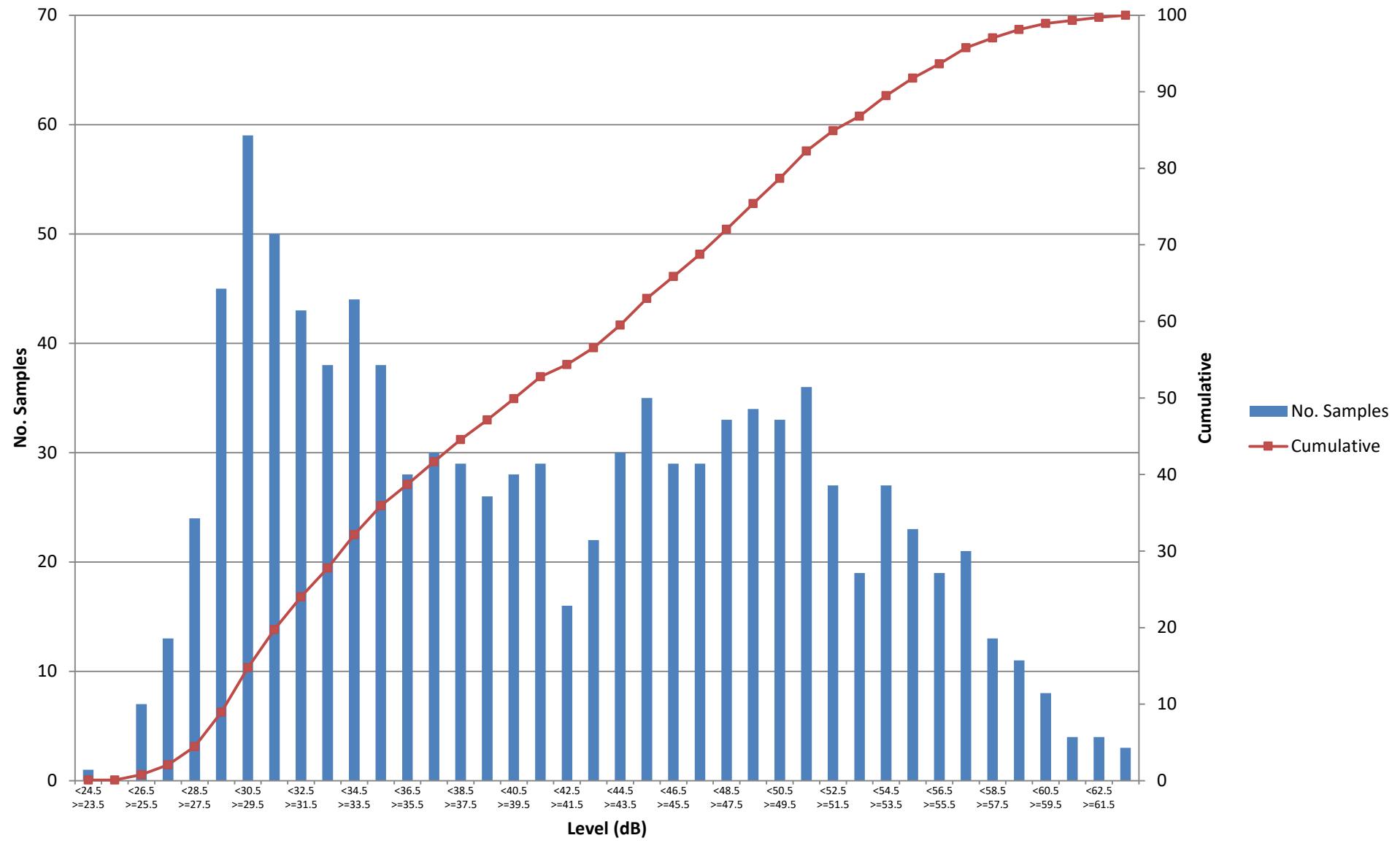
## NMP2 LA90 Daytime Histogram 20/06/25 to 26/06/25



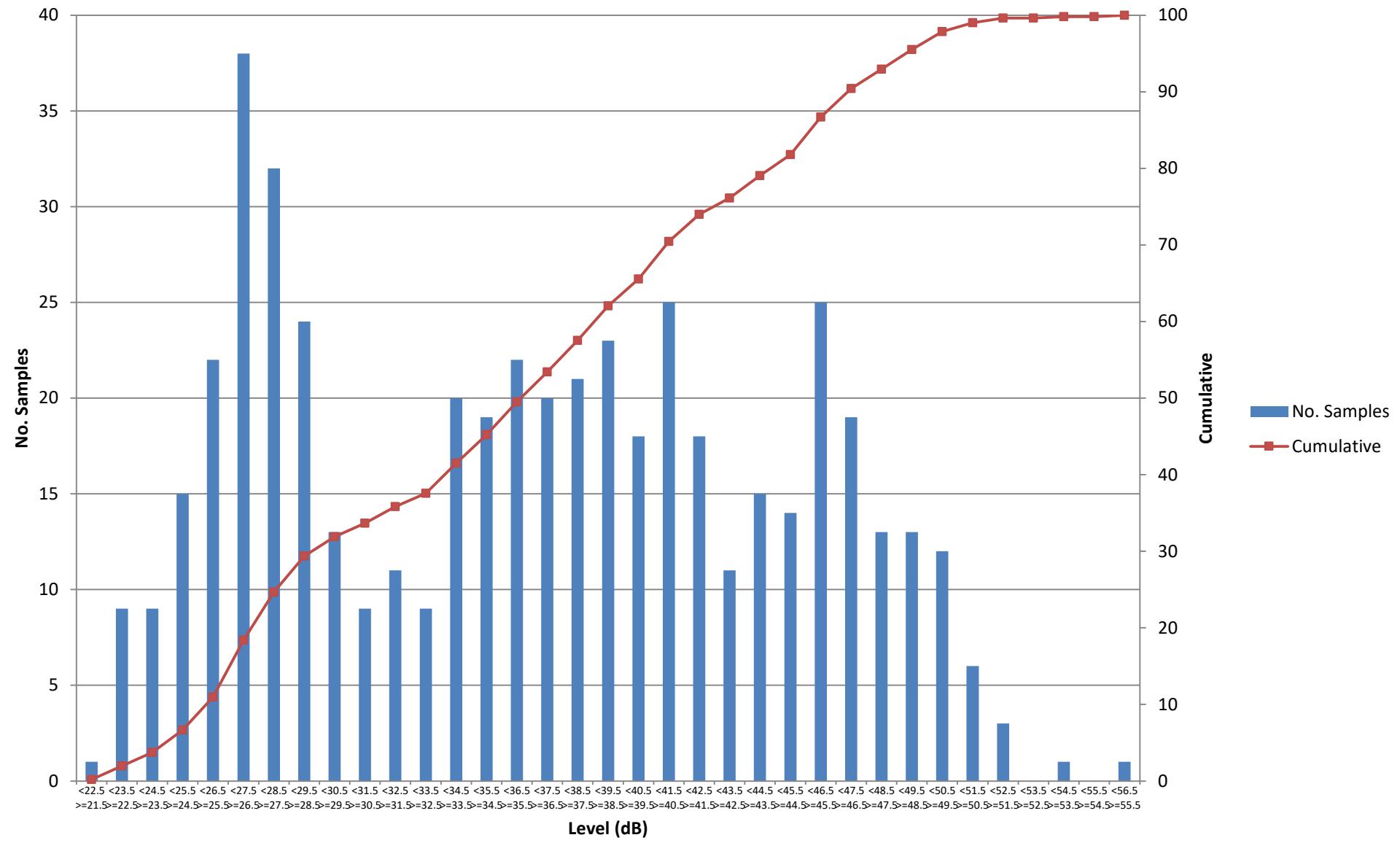
## NMP2 LA90 Night-time Histogram 20/06/25 to 26/06/25



## NMP3 LA90 Daytime Histogram 20/06/25 to 26/06/25



## NMP3 LA90 Night-time Histogram 20/06/25 to 26/06/25



## Annex 2



NSR1 Daytime		15dB										8dB								5dB											
		25 to 125					160 to 400					500 to 10,000						500 to 10,000													
paste here:		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz			
left		-2.1	-3.3	-0.3	-3.9	2.8	12.4	-13.8	0.1	-6.8	-3.8	-2.1	1.3	1.2	-1.4	2.7	-2	-2.4	-2.6	-4.3	-4.6	-7.6	-8.6	-9	-10.9	-10.5	-10				
right		2.1	3.3	0.3	3.9	-2.8	-12.4	13.8	-0.1	6.8	3.8	2.1	-1.3	-1.2	1.4	-2.7	2	2.4	2.6	4.3	4.6	7.6	8.6	9	10.9	10.5	10				
Condition	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE		
	25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz				
A weighted	-10	-7	-6	-1	-1	5	21	10	13	9	7	7	10	13	13	17	16	14	12	7	3	-5	-14	-23	-35	-46	-58				
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5				
Linear	34.5	32.4	29.1	28.8	24.9	27.7	40.1	26.3	26.4	19.6	15.8	13.7	15	16.2	14.8	17.5	15.5	13.1	10.5	6.2	1.6	-6	-14.6	-23.6	-34.5	-45	-55				

TONES

NSR1 Night-time		15dB										8dB										5dB									
		25 to 125					160 to 400					500 to 10,000																			
paste here:		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz			
left		-2.1	-3.2	-0.2	-4	3.1	11.6	-12.9	-0.6	-1.6	-4	-2	0.7	1.1	-1	-0.8	-1.8	-2.1	-3.2	-4.2	-4.3	-6.8	-5.1	-5.7	-8.6	-9.1	-9				
right		2.1	3.2	0.2	4	-3.1	-11.6	12.9	0.6	1.6	4	2	-0.7	-1.1	1	0.8	1.8	2.1	3.2	4.2	4.3	6.8	5.1	5.7	8.6	9.1	9				
Condition	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE			
25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz					
A weighted	-11	-7	-6	-2	-2	5	20	10	12	13	12	12	14	17	17	17	16	15	12	8	4	-3	-8	-15	-24	-34	-44				
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5				
Linear	34.1	32	28.8	28.6	24.6	27.7	39.3	26.4	25.8	24.2	20.2	18.2	18.9	20	19	18.2	16.4	14.3	11.1	6.9	2.6	-4.2	-9.3	-15	-23.6	-32.7	-41.7				

### TONES

NSR2 Daytime																												
paste here:	15dB										8dB																	
	25 to 125					160 to 400					500 to 10,000					2kHz												
	25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz							
	32.8	30.1	26.3	26	21.8	24.5	31.5	23.4	19.4	15.2	11.9	9.2	8.3	8.5	6.6	6.3	4.3	2.2	-1.2	-5.8	-10.1	-16.6	-23.6	-32.8	-48.4	-69.5	-80.1	
left																												
right																												
Condition	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	
	25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz	
A weighted	-12	-9	-8	-4	-4	2	12	7	6	4	3	3	4	5	5	6	4	3	0	-5	-9	-15	-23	-32	-49	-71	-83	
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5	
Linear	32.8	30.1	26.3	26	21.8	24.5	31.5	23.4	19.4	15.2	11.9	9.2	8.3	8.5	6.6	6.3	4.3	2.2	-1.2	-5.8	-10.1	-16.6	-23.6	-32.8	-48.4	-69.5	-80.1	

### TONES

NSR2 Night-time		15dB										8dB										5dB									
		25 to 125					160 to 400					500 to 10,000																			
Condition	25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz				
paste here:	33.2	30.7	27.1	27.0	23.3	25.4	31.5	25.4	20.6	18.9	14.5	11.8	11.0	11.4	8.8	7.5	5.5	3.4	-0.4	-5.0	-9.4	-16.0	-23.0	-32.2	-47.9	-69.3	-80.1				
left		-2.5	-3.6	-0.1	-3.7	2.1	6.1	-6.1	-4.8	-1.7	-4.4	-2.7	-0.8	0.4	-2.6	-1.3	-2	-2.1	-3.8	-4.6	-4.4	-6.6	-7	-9.2	-15.7	-21.4	-10.8				
right	2.5	3.6	0.1	3.7	-2.1	-6.1	6.1	4.8	1.7	4.4	2.7	0.8	-0.4	2.6	1.3	2	2.1	3.8	4.6	4.4	6.6	7	9.2	15.7	21.4	10.8					
A weighted	-12	-9	-8	-3	-3	3	12	9	7	8	6	5	6	8	7	7	6	4	1	-4	-8	-15	-22	-32	-48	-70	-83				
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5				
Linear	33.2	30.7	27.1	27	23.3	25.4	31.5	25.4	20.6	18.9	14.5	11.8	11	11.4	8.8	7.5	5.5	3.4	-0.4	-5	-9.4	-16	-23	-32.2	-47.9	-69.3	-80.1				

TONES

NSR3 Daytime		15dB										8dB										5dB									
		25 to 125					160 to 400					500 to 10,000																			
paste here:		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz			
		35	32.6	29.4	28.7	25.4	26.9	30.7	25.5	20.9	17	15.7	12.8	13.6	14.2	13.7	15.5	13.5	11	8.9	4.9	1	-6	-15	-26.3	-46.1	-74.7	-80.2			
left																															
right																															
Condition	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE		
	25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz				
A weighted	-9.7	-6.8	-5.2	-1.5	-0.8	4.4	11.6	9.4	7.5	6.1	7.1	6.2	8.8	11.0	11.8	14.7	13.5	11.6	9.9	6.1	2.3	-4.8	-14.0	-25.8	-46.2	-75.8	-82.7				
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5				
Linear	35	32.6	29.4	28.7	25.4	26.9	30.7	25.5	20.9	17	15.7	12.8	13.6	14.2	13.7	15.5	13.5	11	8.9	4.9	1	-6	-15	-26.3	-46.1	-74.7	-80.2				

TONES

NSR3 Night-time		15dB										8dB										5dB									
		25 to 125					160 to 400					500 to 10,000																			
paste here:		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz			
		35.0	32.5	29.1	28.4	25.1	26.5	31.0	25.9	21.3	20.9	18.9	16.2	16.8	17.1	16.4	16.2	14.2	11.7	8.9	4.9	1.1	-6.0	-15.0	-26.3	-46.0	-74.7	-80.2			
left		-2.5	-3.4	-0.7	-3.3	1.4	4.5	-5.1	-4.6	-0.4	-2	-2.7	0.6	0.3	-0.7	-0.2	-2	-2.5	-2.8	-4	-3.8	-7.1	-9	-11.3	-19.7	-28.7	-5.5				
right		2.5	3.4	0.7	3.3	-1.4	-4.5	5.1	4.6	0.4	2	2.7	-0.6	-0.3	0.7	0.2	2	2.5	2.8	4	3.8	7.1	9	11.3	19.7	28.7	5.5				
Condition		FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE			
		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz			
A weighted		-10	-7	-6	-2	-1	4	12	10	8	10	10	10	12	14	15	15	14	12	10	6	2	-5	-14	-26	-46	-76	-83			
Correction A-wt		-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5			
Linear		35	32.5	29.1	28.4	25.1	26.5	31	25.9	21.3	20.9	18.9	16.2	16.8	17.1	16.4	16.2	14.2	11.7	8.9	4.9	1.1	-6	-15	-26.3	-46	-74.7	-80.2			

TONES

NSR4 Daytime		15dB												8dB												5dB											
		25 to 125						160 to 400						500 to 10,000																							
paste here:		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz									
left		-2.2	-3	-1.2	-3.1	1.4	6.9	-7.7	-3.6	-4.7	-1.3	-2.8	1	0.8	-0.5	3.9	-1.9	-2.4	-1.9	-3.8	-3.9	-6.5	-8.7	-10.9	-18	-23.7	-16.9										
right		2.2	3	1.2	3.1	-1.4	-6.9	7.7	3.6	4.7	1.3	2.8	-1	-0.8	0.5	-3.9	1.9	2.4	1.9	3.8	3.9	6.5	8.7	10.9	18	23.7	16.9										
Condition	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE								
A weighted	-9	-6	-5	-1	0	5	15	10	9	7	8	7	10	13	13	18	17	16	14	10	7	0	-9	-20	-39	-64	-82										
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5										
Linear	35.3	33.1	30.1	28.9	25.8	27.2	34.1	26.4	22.8	18.1	16.8	14	15	15.8	15.3	19.2	17.3	14.9	13	9.2	5.3	-1.2	-9.9	-20.8	-38.8	-62.5	-79.4										

TONES

NSR4 Night-time		15dB										8dB										5dB									
		25 to 125					160 to 400					500 to 10,000																			
paste here:		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz			
left		-2.1	-3.1	-1	-3.3	1.8	6.1	-6.7	-4	-0.3	-1.3	-2.7	1.2	0.9	-0.5	-0.3	-1.8	-2.4	-2.6	-3.8	-3.9	-6.5	-8.7	-10.9	-18	-23.7	-16.9				
right		2.1	3.1	1	3.3	-1.8	-6.1	6.7	4	0.3	1.3	2.7	-1.2	-0.9	0.5	0.3	1.8	2.4	2.6	3.8	3.9	6.5	8.7	10.9	18	23.7	16.9				
Condition	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE			
A weighted	-10	-6	-5	-1	-1	5	14	11	9	12	13	12	15	17	18	19	18	16	14	10	7	0	-9	-20	-39	-64	-82				
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5				
Linear	35.1	33	29.9	28.9	25.6	27.4	33.5	26.8	22.8	22.5	21.2	18.5	19.7	20.6	20.1	19.8	18	15.6	13	9.2	5.3	-1.2	-9.9	-20.8	-38.8	-62.5	-79.4				

## TONES

NSR5 Daytime		15dB										8dB										5dB									
		25 to 125					160 to 400					500 to 10,000																			
Condition	25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz				
paste here:	34.8	32.6	29.5	28.1	24.9	26.2	32.8	25.2	21.3	17.4	16.1	13.2	14	14.9	14.5	18.1	16.2	13.6	11.6	7.7	3.4	-3.6	-13.1	-25.2	-45.1	-70.4	-80				
left		-2.2	-3.1	-1.4	-3.2	1.3	6.6	-7.6	-3.9	-3.9	-1.3	-2.9	0.8	0.9	-0.4	3.6	-1.9	-2.6	-2	-3.9	-4.3	-7	-9.5	-12.1	-19.9	-25.3	-9.6				
right	2.2	3.1	1.4	3.2	-1.3	-6.6	7.6	3.9	3.9	1.3	2.9	-0.8	-0.9	0.4	-3.6	1.9	2.6	2	3.9	4.3	7	9.5	12.1	19.9	25.3	9.6					
A weighted	-10	-7	-5	-2	-1	4	14	9	8	7	8	7	9	12	13	17	16	14	13	9	5	-2	-12	-25	-45	-72	-83				
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5				
Linear	34.8	32.6	29.5	28.1	24.9	26.2	32.8	25.2	21.3	17.4	16.1	13.2	14	14.9	14.5	18.1	16.2	13.6	11.6	7.7	3.4	-3.6	-13.1	-25.2	-45.1	-70.4	-80				

### TONES

NSR5 Night-time		15dB										8dB										5dB									
		25 to 125					160 to 400					500 to 10,000																			
paste here:		25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz			
		34.8	32.6	29.5	28.1	24.9	26.2	32.8	25.2	21.3	17.4	16.1	13.2	14	14.9	14.5	18.1	16.2	13.6	11.6	7.7	3.4	-3.6	-13.1	-25.2	-45.1	-70.4	-80			
left		-2.2	-3.1	-1.4	-3.2	1.3	6.6	-7.6	-3.9	-3.9	-1.3	-2.9	0.8	0.9	-0.4	3.6	-1.9	-2.6	-2	-3.9	-4.3	-7	-9.5	-12.1	-19.9	-25.3	-9.6				
right		2.2	3.1	1.4	3.2	-1.3	-6.6	7.6	3.9	3.9	1.3	2.9	-0.8	-0.9	0.4	-3.6	1.9	2.6	2	3.9	4.3	7	9.5	12.1	19.9	25.3	9.6				
Condition		FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE			
A weighted		-10	-7	-5	-2	-1	4	14	9	8	7	8	7	9	12	13	17	16	14	13	9	5	-2	-12	-25	-45	-72	-83			
Correction A-wt		-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5			
Linear		34.8	32.6	29.5	28.1	24.9	26.2	32.8	25.2	21.3	17.4	16.1	13.2	14	14.9	14.5	18.1	16.2	13.6	11.6	7.7	3.4	-3.6	-13.1	-25.2	-45.1	-70.4	-80			

### TONES

NSR3 Cumulative Specific																																			
15dB													8dB													5dB									
25 to 125							160 to 400							500 to 10,000									500 to 10,000												
25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz									
paste here:	36.3	33.8	30.4	29.7	26.4	27.8	32.3	27.2	22.6	22.2	20.2	17.5	18.1	18.4	17.7	17.5	15.5	13	10.2	6.2	2.4	-4.7	-13.7	-25	-44.7	-73.4	-78.9								
left		-2.5	-3.4	-0.7	-3.3	1.4	4.5	-5.1	-4.6	-0.4	-2	-2.7	0.6	0.3	-0.7	-0.2	-2	-2.5	-2.8	-4	-3.8	-7.1	-9	-11.3	-19.7	-28.7	-5.5								
right	2.5	3.4	0.7	3.3	-1.4	-4.5	5.1	4.6	0.4	2	2.7	-0.6	-0.3	0.7	0.2	2	2.5	2.8	4	3.8	7.1	9	11.3	19.7	28.7	5.5									
Condition	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE	FALSE								
	25Hz	31.5Hz	40Hz	50Hz	63Hz	80Hz	100Hz	125Hz	160Hz	200Hz	250Hz	315Hz	400Hz	500Hz	630Hz	800Hz	1kHz	1.25kHz	1.6kHz	2kHz	2.5kHz	3.15kHz	4kHz	5kHz	6.3kHz	8kHz	10kHz								
A weighted	-8	-6	-4	-1	0	5	13	11	9	11	12	11	13	15	16	17	16	14	11	7	4	-4	-13	-25	-45	-75	-81								
Correction A-wt	-44.7	-39.4	-34.6	-30.2	-26.2	-22.5	-19.1	-16.1	-13.4	-10.9	-8.6	-6.6	-4.8	-3.2	-1.9	-0.8	0	0.6	1	1.2	1.3	1.2	1	0.5	-0.1	-1.1	-2.5								
Linear	36.3	33.8	30.4	29.7	26.4	27.8	32.3	27.2	22.6	22.2	20.2	17.5	18.1	18.4	17.7	17.5	15.5	13	10.2	6.2	2.4	-4.7	-13.7	-25	-44.7	-73.4	-78.9								

**TONES**